

# **DEVELOPMENT OF A 300 kW<sub>e</sub> INTEGRATED AXIAL TURBINE AND GENERATOR FOR ORC APPLICATIONS**

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ORC Power Systems:  
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# Challenges of Existing Non-Hermetic ORC Systems

## ► Shaft seals

- Generally accepted to be the least reliable component in rotating machinery
- Working fluid leakage is expensive
  - Possibility of fire with flammable refrigerants
  - Must measure and log refrigerant levels
  - Leaked refrigerant replacement is expensive
- Requires shaft seal pressure control system, temperature monitors, leak monitors, etc.
- High inspection and maintenance costs; periodic seal replacement
- Mechanical losses: 1–2%

## ► Gearbox

- Inspection and maintenance costs
- Mechanical losses:  $\approx 4\%$

## ► Couplings

- Inspection and maintenance costs

## ► Lubricated bearings

- Mechanical losses:  $\approx 2\%$
- Requires oil system
- High-speed lubricated bearings have rotordynamics complications

## ► Oil systems

- Use of oil limits the maximum temperature of the heat source
  - High temperatures degrade oil
  - Limits applicability of ORC technology
- Requires oil separator, filter, strainer, and cooler
- Requires periodic oil filter and strainer changes
- Parasitic power losses:  $\approx 2\%$
- High maintenance issues and costs
  - Must measure and log oil levels
  - Periodic oil additions and changes
  - Periodic oil sampling and analysis (moisture, acidity, and metal content)

## ► Instrumentation

- Separate vibration probes and proximity sensors are usually required to monitor turbine and/or gearbox shaft vibration levels on high-speed rotary shafts

## ► Turbine matching

- Standardized turbine designs of many ORC systems are a poor match for many applications

# Effect of Stage Reaction on Turbine Design

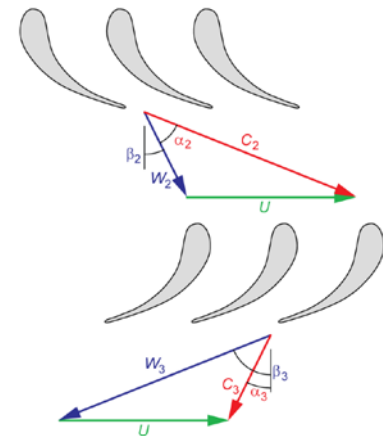
- ▶ Customized ORC turbine designs lead to optimum system efficiency
- ▶ Reaction ( $\Lambda$ ) is a very important parameter in turbine design, fundamentally influencing:
  - Turbine performance characteristics
  - Stator and rotor design
- ▶ Choosing the right reaction is the key to successful design
- ▶ Assuming constant blade speed and meridional velocity, and neglecting internal losses, for a stage of arbitrary reaction, it can be shown that the stage efficiency and specific work output are:

$$\eta = 2v \left\{ (1-\Lambda)^{1/2} \sin \alpha_2 + \left[ (1-\Lambda) \sin^2 \alpha_2 + v^2 - 2v(1-\Lambda)^{1/2} \sin \alpha_2 + \Lambda \right]^{1/2} - v \right\}$$

$$\frac{W_x}{U^2} = \frac{\sqrt{1-\Lambda}}{\Lambda} \sin \alpha_2 + \left[ \frac{1-\Lambda}{v^2} \sin^2 \alpha_2 + 1 - 2 \frac{\sqrt{1-\Lambda}}{\Lambda} \sin \alpha_2 + \frac{\Lambda}{v^2} \right]^{1/2} - 1$$

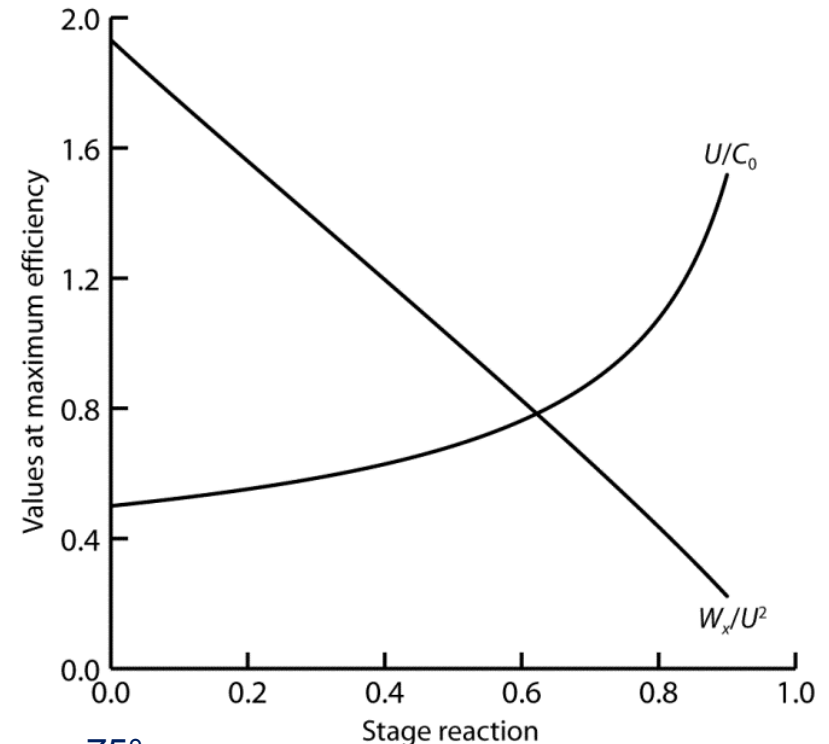
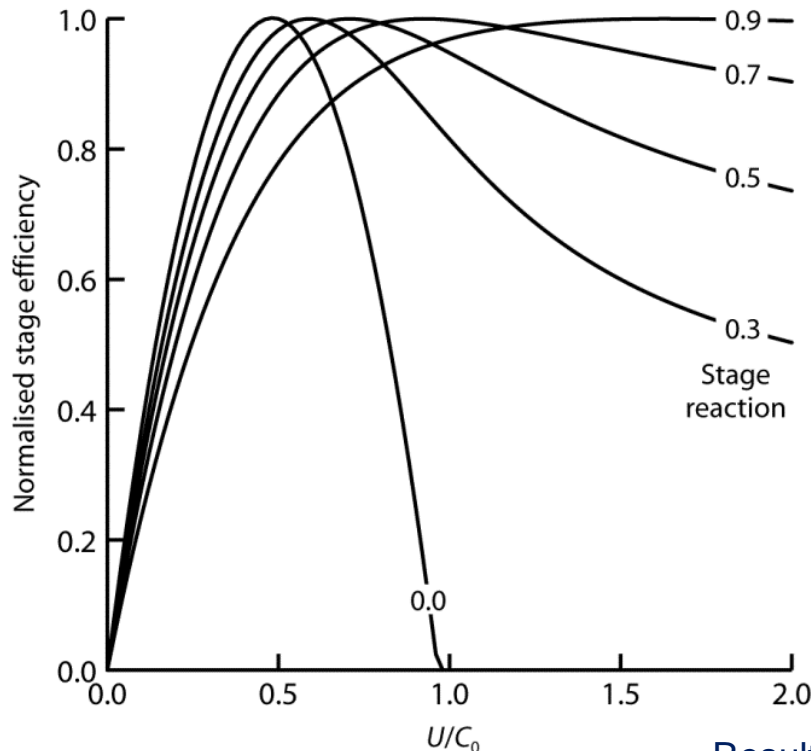
Where:

- $\Lambda$  = Reaction =  $\Delta h_{\text{Rotor}} / \Delta h_{\text{Stage, Stagnation Conditions}}$
- $\eta$  = Stage Efficiency
- $W_x$  = Work, Axial Component
- $U$  = Blade Speed
- $C_2$  = Absolute Velocity, Rotor Stage Inlet
- $W_2$  = Relative Velocity, Rotor Stage Inlet
- $v$  = Velocity Ratio  $U/C_x$
- $\alpha_2$  = Absolute Flow Angle, Rotor Stage Inlet
- $\beta_2$  = Relative Flow Angle, Rotor Stage Inlet



# Stage Reaction Selection Affects Turbine Performance Characteristics

- ▶ Low-Reaction Turbines are generally favored for high-pressure ratio, low-flow applications (i.e., ORC systems), but the choice of reaction depends on many effects – structural, manufacturing, and aero performance
- ▶ Reaction is also influenced by the priorities of high efficiency (→ medium reaction) and high specific work output (→ low reaction)



Results for  $\alpha_2 = 75^\circ$

# **CN's Organic Rankine Cycle Solution Addresses Technical and Economic Issues**

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## ▶ **ORC Turbine Generator Unit (TGU)**

- Consists of: turbine, generator, generator controls, and power electronics

## ▶ **Hermetically sealed 20,000 rpm TGU**

- Axial turbine directly mounted to generator shaft
- No shaft seal, gearbox, or coupling
- Oil-free design

## ▶ **Magnetic bearings**

- No lubricated bearings
- Inherent radial vibrational monitoring

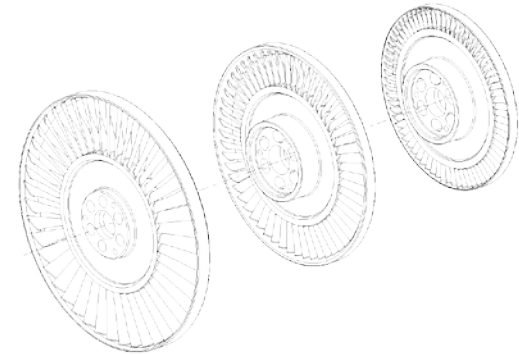
## ▶ **Generator is evaporatively-cooled by refrigerant – patent pending**

## ▶ **State-of-the-art, variable-frequency permanent-magnet generator and controls**

- No speed governor

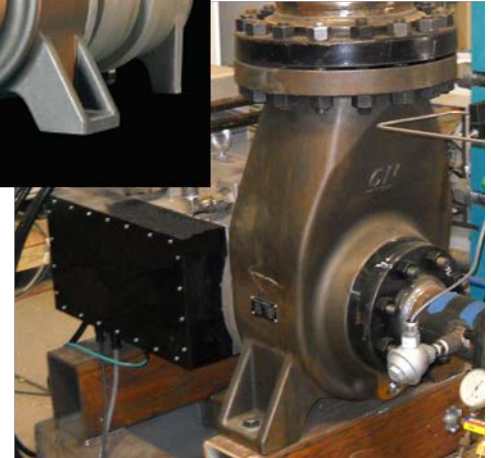
## ▶ **Patent-pending, modular turbine flow path and system**

- Can easily customize a 1- to 4-stage, axial nozzle-rotor subassembly cartridge
- Allows use with a wide variety of working fluids and pressure ratios
- Can meet a customer's exact cycle requirements
- Radial turbine option depending on fluid enthalpy and pressure ratio



# **CN's CN300 ORC TGU Can Operate Over a Range of Conditions**

- ▶ Initial member of CN's ORC TGU product line
- ▶ Designed using CN's Agile Engineering Design System®
- ▶ Gross power range
  - 150–330 kWe
- ▶ TGU speed
  - 20,000 rpm
- ▶ Turbine inlet temperature range
  - 80–220°C
- ▶ Turbine casing inlet pressure rating
  - 40 Bar (Absolute)
- ▶ Turbine casing outlet pressure rating
  - 14 Bar (Absolute)
- ▶ Turbine pressure ratio range
  - 2:1–25:1
- ▶ Working fluid compatibility
  - R112, R113, R114, R134a, R236fa, R245fa
- ▶ TGU size
  - 1.07 m x 0.62 m x 0.87 m
  - 544 kg (1200 pounds)
- ▶ Electrical details
  - 380–480 VAC, 3-phase, 50–60 Hz



Patent Pending



# CN300 Uses Advanced Aerodynamic Design to Optimize Performance

## ▶ **CN's Agile Engineering Design System**

- Ideally suited for ORC turbine applications
- Computer-Aided Engineering (CAE) → Computer-Aided Manufacturing (CAM)

## ▶ **CAE: Aerodynamic analysis**

- Uses CN's AxCent® software
- For complex blade geometries
- Interfaces with third-party optimizers

## ▶ **Multistage 3D CFD analysis**

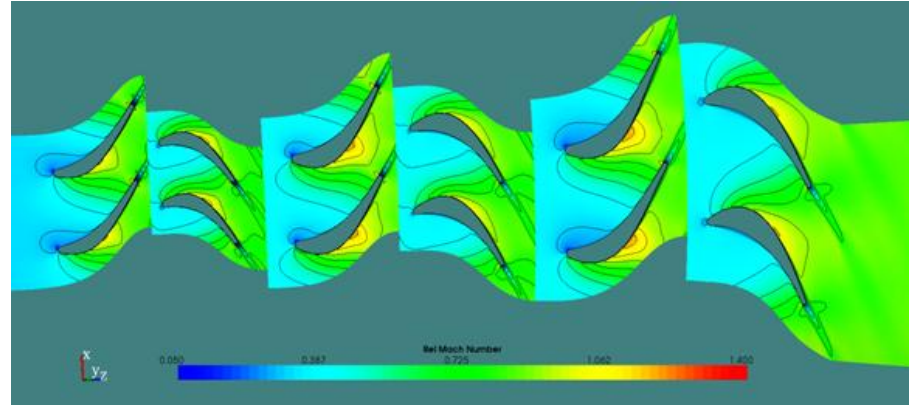
- Allows accurate performance prediction of entire unit
- Allows improved stage matching
- Better resolution of 3D effects and secondary flows

## ▶ **Custom, optimized design**

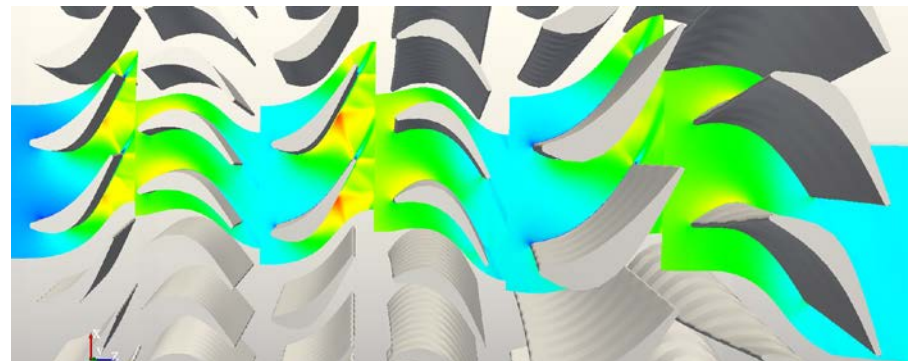
- Optimized for each customer application
- 1 to 4 expansion stages
- Choice of refrigerants and conditions

## ▶ **Calculate performance of existing CN300 design with new customer conditions**

- Avoid nonrecurrent engineering



Typical CFD Turbine Analysis Results



Mach Number Contours Through Flow Path

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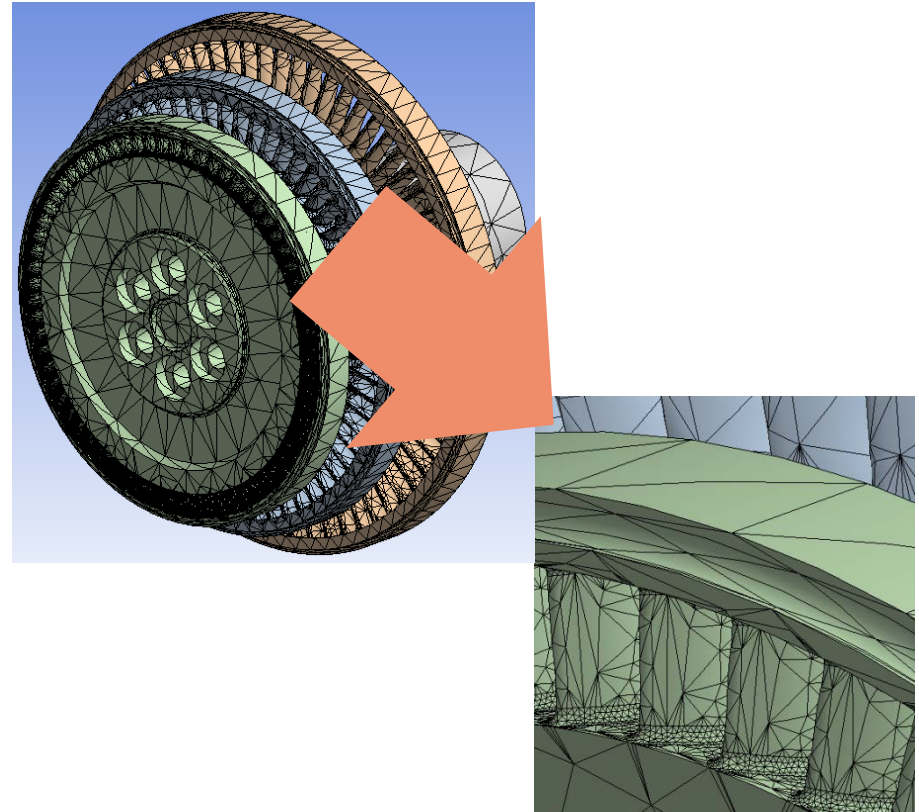
# CN300 Mechanical Design Uses Advanced Design Techniques

## ► CAE-based Finite Element Analysis (FEA)

- FEA models created in ANSYS® Workbench™
- Blade stacking of 2D cross sections
- Blade restaggering around an arbitrary axis
- Bowed blading defined by hub-to-shroud bow profiles
- And more

## ► Also developed specifications and methodology for Selective Laser Sintering (SLS) process

- For rotors and stators
- Good alternative to 5-axis machining
- Complexity of airfoil shape is not limited by machining (i.e., flank milling vs. point milling)



Mesh and Mesh Detail for FEA

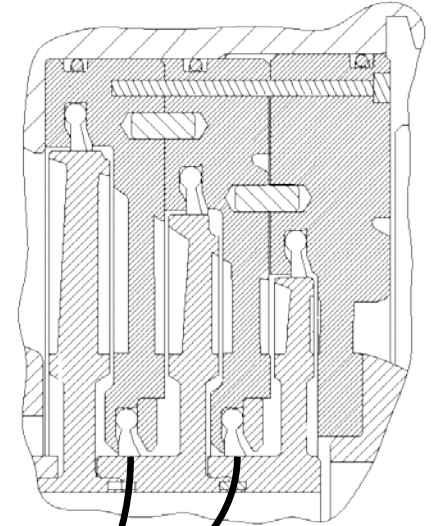
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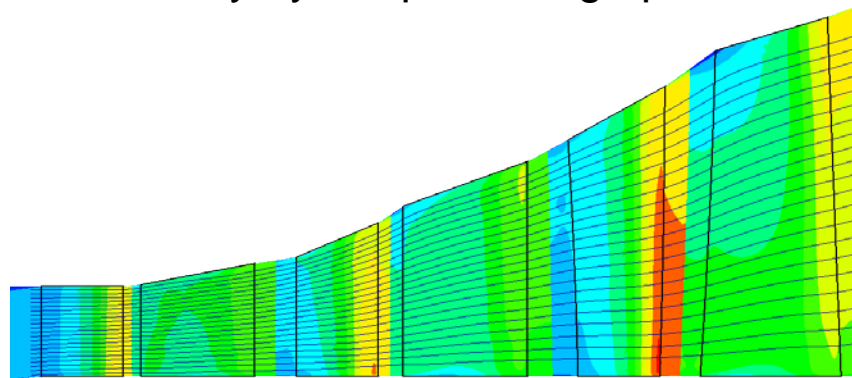
# Brush Seals Markedly Improve CN300 Performance

## ► Brush seals – patent pending

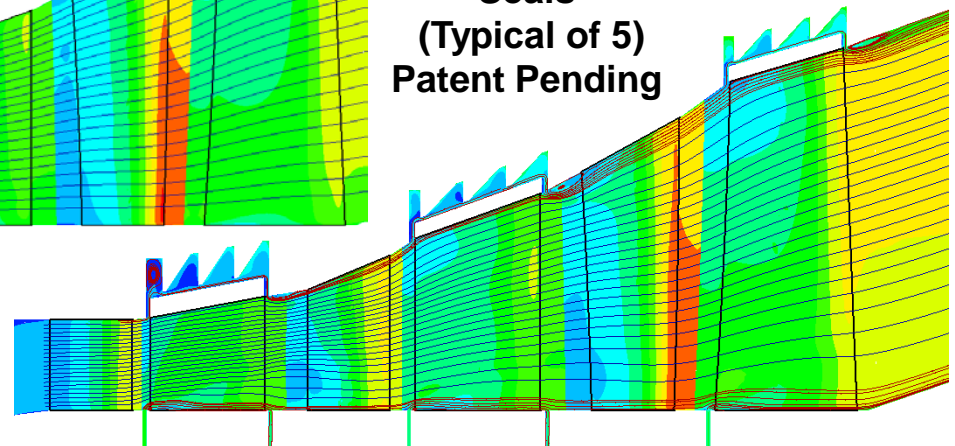
- Used since the early 1980s in aircraft engines
- Used since the mid-1990s in gas and steam turbines
- Installed on rotor and stator
- Significant impact on ORC CN300 performance
  - Reduce gas leakage by 97.8%
  - Improve efficiency by 3.7 percentage points



**No Leakage  
(Ideal Brush Seal)**



**Leakage with  
Labyrinth Seal**



**Brush  
Seals  
(Typical of 5)  
Patent Pending**

# **CN's Combination of Advanced Design Features Lead to a State-of-the-Art Unit**

- ▶ **Previous ORC system limitations resolved**
  - New CN300 TGU = hermetic, direct-drive, oil-free, magnetic bearings, refrigerant-cooled, no speed governor
- ▶ **CN300 design goal: Zero maintenance**
  - Reduced operating/maintenance costs
  - Reduced project lifecycle costs
  - Maximized TGU efficiency
- ▶ **CN300 design criteria: Easily customized flow path design**
  - For various heat sources, temperatures, and working fluids
  - To maximize turbine efficiency
  - To maximize client project revenue
- ▶ **Now commercially available**



Finished Machined Rotor  
(one of three used in the CN300 system)